midwest engineering services, inc.







March 26, 2007

Mr. Jerry Killian, Administrator City of Prescott 800 Borner Street Prescott, Wisconsin 54021

SUBJECT: Subsurface Exploration and Geotechnical Analysis

TID #5 Improvements Prescott, Wisconsin MES Project No. 4-73027

Dear Mr. Killian.

The subsurface exploration and analysis for the referenced project has been completed. Two (2) copies of the report are included herein, and one (1) copy has been forwarded to Mr. David Schofield of Cedar Corporation.

After you have had the opportunity of reading the report, please call at any time with any questions or comments you may have. Midwest Engineering Services, Inc. (MES) appreciates the opportunity to be of service on this project, and looks forward to continuing as your geotechnical consultant during the design and construction phases, as well as your upcoming projects.

Sincerely,

MIDWEST ENGINEERING SERVICES, INC.

Jeffrey A. Manninen Branch Manager

James M. Becco, P.E. Region Manager

SUBSURFACE EXPLORATION AND GEOTECHNICAL ANALYSIS

TID #5 Improvements

Prescott, Wisconsin

Prepared for

City of Prescott

800 Borner Street

Prescott, Wisconsin 54021

MES Project No. 4-73027

March 26, 2007

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INTRODUCTION

General

This report presents the results of the subsurface exploration and analysis for the street and utility construction for the proposed industrial park in the City of Prescott, Wisconsin. The work was performed for the City of Prescott, at the request of Mr. David Schofield of Cedar Corporation.

Purpose

The purpose of this study was to determine and evaluate the subsurface conditions at the site, and to establish parameters for use by the design engineers in preparing the utility and pavement designs for the proposed project. Preliminary foundation recommendations have also been included. However, a comprehensive foundation evaluation, and recommendations for specific lots or structures, was beyond the scope of this report.

Scope

The scope of services included a site reconnaissance, the subsurface exploration, a determination of soil characteristics by field and laboratory testing, and an evaluation and analysis of the data obtained. The scope of the field exploration program, including the number, depth and approximate location of the borings, was determined by Cedar Corporation.

Authorization

The description of services and authorization to perform this subsurface exploration and analysis were in the form of a signed copy of MES Proposal No. 4-7025, dated February 22, 2007. This subsurface exploration and analysis report has been prepared on behalf of and exclusively for the use of the City of Prescott. The information contained in this report may not be relied upon by any other parties without the written consent of MES, and acceptance by such parties of MES' General Conditions.

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SITE AND PROJECT DESCRIPTION

Site Features and Project Description

The proposed project will consist of the construction of new roads and utilities for a planned industrial park which will be located on the northeast corner of the intersection of USH 10 and STH 29/35; and on the southeast corner of the intersection of USH 10 and Dexter Street, in Prescott, Wisconsin. At the time of the subsurface exploration, the subject site generally consisted of vacant fields. Some grading had been performed on the south side of USH 10, in preparation of the new roads.

Exact utility invert depths had not been determined at the time of this report preparation. However, it is understood that the sanitary sewer lines located on the north and south sides of USH 10 will be installed to maximum depths of about 20 and 30 feet below existing grades, respectively. It is understood that the roads located on the north side of USH 10 will be about 3 to 5 feet lower than existing grades, and that the grades of the roads on the south side of USH 10 will be similar to existing ground surface elevations. It is understood that the new buildings located within the industrial park will utilize slab-on-grade construction, and will not have basements.

EXPLORATION PROCEDURES

Scope Summary

The field and laboratory data utilized in the evaluation and analysis of the subsurface materials was obtained by drilling exploratory test borings, securing soil samples by the split-spoon sampling method, and subjecting the samples to laboratory testing.

Field Exploration

Seventeen (17) soil borings to a depth of about 20 feet (B-1 through B-17), and four (4) soil borings to a depth of about 30 feet below ground surface (B-18 through B-21), were planned for this project. However, auger refusal, due to sandstone, was encountered in seventeen (17) of the borings (B-1 through B-7, B-10, B-11, B-13 and B-15 through B-21) at depths of about 6.5 to 18.6 feet (EL 842.0 to EL 894.8). Cedar Corporation staked the boring locations and provided ground surface elevations.

The soil test borings were performed with a truck-mounted rotary drilling rig utilizing continuous flight hollow stem augers (HSA) to advance the boreholes. Representative soil samples were obtained by the Standard Penetration Test (SPT) method in general accordance with ASTM D-1586 procedures. The SPT soil samples were transferred into clean glass jars immediately after retrieval, and returned to the laboratory upon completion of the field operations.

A copy of the Soil Boring Logs and the Boring Location Diagram are included in the Appendix. The soil stratification shown on the logs represents the soil conditions at the actual boring locations at the time of the exploration. The terms and symbols used on the logs are described in the General Notes found on the last page of the Appendix. After completion of the borings, the boreholes were backfilled to the ground surface with bentonite chips.

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Laboratory Testing

Soil samples obtained from the exploration were visually classified by a soils engineer in the laboratory, and subjected to testing, which included moisture content determination testing, percent finer than the No. 200 sieve, and Atterberg Limits determination. The laboratory

testing was performed in general accordance with respective ASTM methods, as applicable, and the results are shown on the boring logs in the Appendix.

DESCRIPTION OF SUBSURFACE CONDITIONS

General

A description of the subsurface conditions encountered at the test boring locations is presented on the Soil Boring Logs. The lines of demarcation shown on the logs represent an approximate boundary between the various soil classifications. It must be recognized that the soil descriptions are considered representative for the specific test hole locations, but that variations may occur between and beyond the sampling intervals and boring locations. The soil depths; surficial topsoil, fill and layer thicknesses; and demarcation lines can be used for preliminary construction calculations, but should not be expected to yield final and exact quantities. A summary of the major soil profile components is described in the following paragraphs.

Soil Conditions

The surface of the site at borings B-1 through B-17 is covered with about 7 to 21 inches of topsoil. The surface at borings B-18 through B-21 is covered with about 6 to 19 inches of fill materials, consisting of mixtures of clayey sand; and silt, which had been placed in preparation of new roads. These surficial soils are generally underlain by natural granular strata comprised of silt and sand, with varying amounts of clay and gravel, to depths ranging from about 1.7 to 21.5 feet (EL 844.7 to EL 897.6). These soils may be considered very loose to very dense, with standard penetration resistances between 2 to 47 blows per foot, and natural moisture contents ranging from 1 to 16 percent. It should be noted that 2 to 7.5 foot thick clay layers were encountered in borings B-5 and B-14, at depths of about 5 and 12.5 feet (EL 883.2 and EL 853.7), respectively.

At each of the borings, with the exception of B-9 and B-14, the granular soils were underlain by sandstone, to at least the termination depths of the borings (6.5 to 21.5 feet / EL 842.0 to EL 894.8). These materials were generally in a very dense condition. As previously noted, the drill rig experienced auger refusal, due to the sandstone, in all of these borings with the exception of B-8 and B-12. However, in some areas, the upper portions of the sandstone was more weathered, and the drill rig was able to penetrate it several feet with the augers.

To aid in the determination of asphalt pavement coefficients, laboratory testing was performed on two (2) samples obtained from the borings. A composite sample of sandy silt, obtained from a depth of about 2.5 to 4 feet below ground surface at borings B-1, B-5 and B-7, was subjected to percent finer than the No. 200 sieve and Atterberg Limits determination. Results of the testing indicate a non-plastic soil, with a percent passing the No. 200 sieve of 81. This soil has an AASHTO classification of A-4.

A sample of silty, clayey sand, obtained from the upper 10 to 19 inches of borings B-18, B-19 and B-20, was also subjected to percent finer than the No. 200 sieve and Atterberg Limits determination. Results of the testing indicate a relatively low-plasticity soil with a Plasticity Index of 9 and a percent passing the No. 200 sieve of 39. This soil also has an AASHTO classification of A-4.

The foregoing discussion of soil conditions on this site represents a generalized soil profile as determined at the test boring locations. A more detailed description and supporting data for each test location can be found on the individual Soil Boring Logs.

Groundwater Observations

Groundwater observations were made during drilling operations and in the open boreholes upon completion. No free water was encountered in any of the boreholes while drilling or upon completion.

On the basis of the field observations and the soils relative moisture contents, the free water level is judged to be below the depth of the borings at the time of the exploration. However, it must be recognized that groundwater levels fluctuate with time due to variations in seasonal precipitation, lateral drainage conditions, and soil permeability characteristics.

EVALUATION AND RECOMMENDATIONS

General

On the basis of the data obtained in this exploration, the soils encountered in the borings below the topsoil are generally considered suitable for the support of new structures, utilities and pavements. However, some of the on-site soils exhibited relatively low strength characteristics, and therefore, dependent upon the locations and development grades selected for new structures and utility lines, some overexcavation and/or recompaction/replacement of bearing soils may be required. A thorough subsurface exploration and foundation evaluation must be performed within the building footprints to determine site-specific recommendations for each structure, as planning progresses.

Very dense sandstone was encountered above the planned maximum depths of the utility inverts within all but two (2) of the soil borings (B-9 and B-14). The following table indicates the approximate elevations that sandstone was encountered, the approximate elevations where drilling refusal was encountered, and the elevations of the planned deepest utility bottom at that location.

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Boring	Approximate	Approximate	Estimated Elevation
Number	Elevation of	Elevation of Auger	to Approximate Pipe
	Sandstone (ft.)	Refusal (ft.)	Invert (ft.)
B-1	845.1	842.0	840.6
B-2	862.1	854.1	850.1
B-3	869.3	869.0	855.5
B-4	870.2	866.1	856.2
B-5	881.2	874.1	868.2
B-6	895.4	894.8	887.4
B-7	897.4	894.3	892.4
B-8	910.9	-	909.4
B-10	891.1	888.0	879.6
B-11	874.2	872.1	863.2
B-12	844.8	20	844.8
B-13	860.9	860.1	847.9
B-15	863.1	858.1	850.1
B-16	861.8	855.1	849.8
B-17	895.2	892.6	882.7
B-18	893.3	886.0	866.1
B-19	886.1	878.0	861.1
B-20	891.8	884.3	863.4
B-21	879.5	871.1	851.3

Based on this, extremely difficult excavating, requiring blasting or other rock removal methods, will be encountered.

Utility construction must be performed in accordance with "The Standard Specifications for Sewer and Water Line Construction for the State of Wisconsin." A discussion of construction guidelines and recommendations is included in the following sections.

Site Preparation

The presence of organic topsoil and surface vegetation in the subgrade can adversely affect the serviceability of structural fills, foundations, floor slabs, pavements and other structures placed upon them. To reduce the potential for detrimental settlements, the general site preparation in these areas must include the removal of these items along with any other deleterious materials encountered. On the basis of the data obtained from the borings, the estimated depth of topsoil removal will range from about 7 to 21 inches. However, some variation should be expected between and beyond the boring locations.

In the areas of planned buildings, roads, driveways, sidewalks, or other structures, subsequent to stripping of the topsoil and cutting to planned grades, the resulting subgrade must be thoroughly proofrolled during dry weather conditions to detect unstable, yielding soils which

must be removed or improved by appropriate preparation and compaction techniques. The upper soils across the site have high amounts of fines (silt and clay) which make them very sensitive to moisture. As such, it is anticipated that if construction is carried out during periods of cool and/or wet weather, it will be difficult to create a stable working subgrade in some areas. Scarification and drying of wet soils or removal and replacement with suitable fill are two methods which can be considered when unstable conditions are encountered, but this should be determined by the soils engineer at the time of construction.

Prior to the placement of pipe, or before any supporting fill is placed, the loose or obviously compressive materials must be removed. Any isolated areas of excessive yielding should be excavated and backfilled with clean, compacted soil.

In planned areas of overlying structures (beneath roads, driveways, light poles, utilities or other structures), any fill used above the pipe bedding and cover material should ideally be a clean, granular material. In general, portions of the on-site sand soils are considered suitable for reuse as structural fill, subject to proper moisture control. However, the soils containing high amounts of fines, present in most areas, are highly moisture sensitive and will be extremely difficult to re-use as backfill if they become wet. Additionally, excavated or blasted sandstone is not likely to be suitable for re-use as backfill, unless it is crushed to proper size. The use of imported granular fill may be required, and extensive quantities may be needed in some areas.

Fill in structural areas should be placed in maximum twelve (12) inch loose lifts (except that the first layer above the pipe can be increased to 24 inches in thickness) and be compacted to 95 percent of ASTM-D698 (Standard Proctor). The selection of fill materials for various applications should be done in consultation with the soils engineer.

Proper moisture control is essential to reduce the amount of compactive effort necessary to achieve the desired densities. This is especially true of clayey and silty soils, where scarification and aeration may be required to achieve near-optimum moisture levels prior to compaction. Small hand-operated compactors, such as jumping-jack type, should be used in confined areas and granular fills are generally more readily compacted to the required densities in such applications.

Preliminary Foundation Recommendations

The following is a general overview of the subsurface conditions for the site, as it relates to foundation analysis, and can be used in preliminary site planning. It is recommended that a more in-depth investigation be conducted prior to construction to determine specific recommendations for each particular structure.

In general, typical one or two-story commercial buildings may be supported by a conventional spread footing system, bearing on suitable naturally occurring soils or within structural fill, if soil conditions and development grades allow. Based on the data obtained in the soil borings for this preliminary study, some of the naturally occurring soils encountered beneath the topsoil at

the boring locations, are considered suitable for direct foundation or structural fill support. However, some of the soils are in a very loose to loose condition, and therefore, dependent upon the locations and development grades selected, some overexcavation and recompaction/replacement and/or extension of foundations may be required.

It is anticipated that conventional spread footings and continuous wall footings bearing upon the naturally occurring soils encountered in the upper levels of the borings, or upon structural fill placed to form a suitable subgrade, could be designed for a net allowable soil bearing pressure in the range of 1,000 to 4,000 PSF. However, this will be dependent upon the locations of the structures, and bearing elevations.

Silty and clayey (high fines content) soils are highly moisture sensitive, and are therefore subject to significant softening and yielding when the confining effect of the overburden is removed. If soft or unstable areas are observed at the time of construction, it may be necessary to remove the soils and replace them with compacted structural fill, possibly in conjunction with the use of a crushed stone working mat. It is recommended that the footing excavations be observed by a representative of the soils engineer at the time of construction to evaluate the bearing subgrade.

Since cutting and filling will likely take place for the site grading, the subgrade must be properly prepared prior to filling activities, and all fill must be placed in a controlled manner. This should be monitored and tested by a representative of the soils engineer. Recommendations for subgrade preparation and compaction were presented in a previous section of this report.

In general, the performance of foundation systems on this site will be dependent on the various factors discussed herein. The soil bearing pressures suggested herein should be used for preliminary planning only, in the evaluation of general site feasibility. As indicated previously, additional soil borings are recommended when the final structure locations have been determined.

Pipe Material

In order to reduce the amount of pipe deflection, it must be recognized that proper selection and compaction of the pipe bedding and cover materials is essential. This should be done in accordance with the standard specification for sewer construction. Bedding material exhibiting a well defined moisture density relationship must be compacted to 95 percent of ASTM-D698 (Standard Proctor).

In general, the pipe and associated manholes, bearing upon medium dense to very dense granular soils, can be designed to exert a net allowable bearing pressure of 3000 psf. However, dependent upon the invert locations selected, the removal and replacement of natural low-strength soils may be required. If blasting is required, the removal and replacement of larger blastrock, and/or the use of a vibratory plate compactor within the bottoms of the excavations may be required prior to pipe placement. It may also be necessary

to remove soft or loose overburden soils which have sloughed into the excavation from the sidewalls during the blasting activities. A suitable and stable subgrade must be present prior to the placement of piping or bedding materials.

Trench Backfilling

Backfilling of the pipe and trench should be performed in accordance with the applicable chapters of the *Standard Specification for Sewer and Water Line Construction*. This will be dependent on the type of pipe selected, embedment depth and other factors.

It is recommended that well graded granular soils such as those specified in Tables 37 and 39 of the *Standard Specification for Sewer and Water Construction* be utilized as backfill in utility trenches to reduce the potential for consolidation and settlement of the backfill. All fill soils must be placed and compacted in accordance with the site grading specifications under engineering controlled conditions, to provide suitable support for overlaying structures and roadways. Silt and clay soils are not recommended for reuse as backfill within utility trenches due to the substantial difficulty of obtaining proper compaction in confined areas.

Placement of bedding and cover material shall be sufficient to protect the type of pipe selected as specified by the pipe manufacturer. Trench backfill should be placed in layers not more than 12 inches in loose thickness before compaction, except that the first lift of backfill placed over the pipe can be increased to 24 inches if necessary to protect the pipe from compaction equipment. Subsequently thinner lifts may be required depending on the type and size of compaction equipment available.

Each lift of backfill above the pipe bedding and cover, especially in areas of overlying structures (pavement, sidewalks, light poles, etc.) must be compacted to a density of at least 95 percent of the maximum dry density as determined by the Standard Proctor method (ASTM D698).

CONSTRUCTION CONSIDERATIONS

Groundwater Control

Because no groundwater was encountered in the borings during the exploration, no major groundwater-related difficulties are anticipated during excavation and construction of the proposed shallow foundation system. A gravity drainage system and filtered sump pumps, or other conventional dewatering procedures, should be adequate to control perched water if encountered during shallow excavation work.

While no groundwater was encountered at the time the borings were drilled, it should be noted that seasonal changes in precipitation and site drainage conditions can cause accumulation of free water in the upper levels. Additionally, extensive zones of groundwater (not disclosed by

the borings) can be present within caverns or other pockets below the bedrock surface. If such are encountered where deep excavations into bedrock are necessary, a series of well points and/or high volume pumps with sufficient lifting capacity, along with support of excavation side walls (within the overburden) with shoring and bracing or sheet piling, may be required to maintain dry conditions to permit proper construction, and the placement and compaction of backfill.

Excavations

Due to the presence of granular soils, and the planned depth of sewer and water construction, the use of shoring, bracing, and/or sloping will be required. Excavations for utilities may require the flattening of side slopes to at least 1.5 H to 1.0 V. To reduce the volume of soil to be removed it may be beneficial to use a trench box in combination with flattening of the side slopes, depending on the actual depth of the excavation. Where a combination of flattening slopes with a trench box is selected, the toe of the slope of the upper portion must start 1.5 feet below the top of the trench box.

Sandstone was encountered in the majority of the borings, at depths ranging from about 1.6 to 20 feet (EL 844.8 to EL 897.4). As previously noted, the drill rig experienced auger refusal, due to the sandstone, in seventeen (17) of the borings, at depths ranging from 6.5 to 18.6 feet (EL 842.0 to EL 894.8). However, at most of the borings, the drill rig was able to penetrate several feet into the more weathered materials, above the refusal depths. A qualified contractor, using proper equipment and ripping techniques, may be able to excavate at least the upper portions of the sandstone in some areas. However, difficult digging and longer excavation times should be expected. In addition, considering the refusal depths and the corresponding invert elevations, blasting will likely be required in some areas. This must be performed by an experienced contractor, utilizing proper care to avoid damage to nearby buildings, utilities, or other structures. It is recommended that test pits be performed as part of preconstruction planning to further evaluate the excavatability and surface elevations of the sandstone. It is also recommended that photographic and/or video documentation of the condition of nearby buildings, utilities, and other structures be made prior to any blasting.

Since the subgrade overburden soils are generally sensitive to moisture, every effort should be made to provide adequate drainage across the site during construction, and to prevent runoff from infiltrating excavations. These soils are also subject to erosion caused by runoff, and erosion control measures should be implemented where needed or required by local ordinances. All excavation work must be performed in accordance with applicable federal and state OSHA codes, and as necessary to protect life and property.

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Seismic Design Parameters

Natural soils encountered at the test boring locations generally had moderate strength characteristics. The site is therefore considered to be Seismic Class C, based on Table 1615.1.1 of the 2000 International Building Code.

PAVEMENT DESIGN RECOMMENDATIONS

Based on the existing and expected grades across the project site, and the subgrade conditions encountered at the boring locations, the pavement subgrade will generally consist of silt, with varying amounts of sand, on the north side of USH 10; and of silty, clayey sand, with sandstone fragments, on the south side of USH 10. Two (2) samples were subjected to laboratory testing. A composite sample, obtained from a depth of about 2.5 to 4 feet below ground surface at borings B-1, B-5 and B-7 (located on the north side of USH 10) was subjected to percent finer than the No. 200 sieve and Atterberg Limits determination. Results of the testing indicated a non-plastic soil, with an AASHTO classification of A-4. A sample of silty, clayey sand, obtained from the upper 10 to 19 inches of borings B-18, B-19 and B-20 (located on the south side of USH 10) was also subjected to percent finer than the No. 200 sieve and Atterberg Limits determination. Results of the testing indicate a relatively low-plasticity soil which also has an AASHTO classification of A-4.

These soils are generally rated as poor for pavement subgrade support based upon their low to moderate shrink/swell potential, moderate to high frost susceptibility, and poor drainage characteristics. They have a Frost Index of F-4, Design Group Index of 16, Soil Support Value of 3.5, and Subgrade Modulus of 150 pci.

Analysis of the visual classification and laboratory testing has been made in determining pertinent engineering properties of the subgrade soils, as described in the Wisconsin Soils Manual for Pavement Section Design. Any new fill brought to the site to raise the existing grade must be of comparable or better quality than the A-4 soils reported herein.

PAVEMENT SUBGRADE DESIGN COEFFICIENTS

AASHTO Soil Classification	A-4
Drainage	Poor
Shrink/Swell Potential	Low to Moderate
Design Frost Index	F-4
Design Group Index	16
Soil Support Value	3.5
Estimated Subgrade Modulus (k)	150

GENERAL COMMENTS

This geotechnical exploration analysis has been prepared to aid in the evaluation of the subsurface conditions on this site. The recommendations presented herein are based on the available soil information and the design information provided. Any changes in the design information should be brought to the attention of the soils engineer to determine if modifications in the recommendations are required. A soils engineer should also review the final design plans and specifications to determine that the recommendations presented herein have been interpreted and implemented as intended.

This geotechnical study has been conducted in a manner consistent with that level of care ordinarily exercised by members of the profession currently practicing in the same locality under similar conditions. The findings, recommendations and opinions contained herein have been promulgated in accordance with generally accepted practice in the fields of foundation engineering, soils mechanics, and engineering geology. No other representations, expressed or implied, and no warranty or guarantee is included or intended in this report.

It is recommended that the earthwork and backfill operations be monitored by the soils engineer, to test and evaluate the soil capacities, and the selection, placement and compaction of controlled fills.

APPENDIX

Appendix (in order of appearance)
Figure 1 — Boring Location Plan
Soil Boring Logs
General Notes

SOIL BORNO 1 201 HOW HOS \$70.1 \$ 375.52 SOIL BORNG 3 SFREET Sour BORNO 13 Soul BORNO 18 JAMES STREET PINE PINE \$76,20 \$00, BORNIG 4 INDUSTRIAL 38-33 PARK Or 92 39 5 107 9 SERMENTREET SOIL BORING 5 11 ONEHOR TICS ימון ניום tor. ä 883.22 ST. DEXTER \$99.58 **SON. BORING 10 Sof Borato 18 SOL BORNO 6 ¥501, BORNG 21 902.68 Son, Bornyo 17 **SON BORRUG 19 78. AH SOIL BORNG 7 U.S.H. 10 ¥504, BORNG 20 893.36 919.06 424.42 SOIL BORNG B

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NOTE: B-18 WAS OFFSET 45' SOUTH, B-18 WAS GFFSET 80 SOUTH AND B-21 WAS OFFSET 30' EAST, SO THEY COULD E PERFORMED WITHIN PLANNED ROADS, AS PER CEDAR CORP.

(DRAWING PROVIDED BY CEDAR CORP.)

) DATE: 3-26-07

FIGURE 1
BORING LOCATION PLAN
TID #5 IMPROVEMENTS
PRESCOTT, WISCONSIN

PROJECT NO.: 4-73027



Project No.: 4-73027

Project: Location:	TID #5 Improvements Prescott, Wisconsin	Dri	ili Date:	4-73027 March 9, 2007 Joe Black
DERTHIEL	VISUAL SOIL CLASSIFICATION	SAMPLE N	Qp	Qu MC

DEP	TH/EL.	VISUAL SOIL CLASSIFICATION	SAMPLE	N	Qp	Qu	мс	DEMARKS	
1	feet)	GROUND SURFACE ELEVATION: 860.6	NO.	(bpf)	(tsf)	(tsf)	(%)	REMARKS	
, -	859.6	0-13": Dark grayish brown SILT, with clay, trace sand (TOPSOIL)	1-AU						
2 3	858.6		1-70		L				
	857.6	Out to be the same and to Old T. trace after a down		-	-				
Ĭ	856,6	Grayish brown sandy SILT, trace clay, damp	2-SS	5			16		
٦	855.6								
-	854.6		3-88	5			16		
	853.6	Dark brown sandy SILT, trace clay, damp						7	
7 -	852.6		_			—		·	
"=	851.6		4-88	9			13		
₁₀ " =	850.6	Brown sandy SILT, little clay, damp							
	849.6		5-SS	7			12		
"-	_						<u> </u>	1	
12	848.6				,				
13-	847.6	Brown silty SAND, little gravel, moist						1	
14 — 15 -	845.6							1	
	-		6-88	25				. 7	
16-	844.6		0-00	20				1	
17-	843.6	Tan to light gray weathered SANDSTONE						1	
18 -	842.6		7-SS \	50/1"				-	
19 -	841.6							1	
20	840.6	END OF BORING @ 18.6± FEET						-	
21 -	839.6	(Auger refusal at 18.6 feet due to sandstone)						1	
22 _	838.6	(Adder related of 10.0 foot and to option of						4	
23 —	837.6							-	
24	836.6							4	
25	835.6							-	
26 _	834.6							4	
27	833.6					ĺ		4	
28 _	632.6					ı		4	
29 _	831.6						I	4	
30	830.6								
31_	829.6			Ì		I		4	
32_	828.6					- 1	- 1	4	
33_	827.6						- 1	4	
34	826.6					l	- 1	4	
35	825.6					I			
36_	824.6]	I	i		4	
37_	823.6				l	- 1		4	
38	822.6				I	l	l	4	
39_	821.6_				Ì		I	4	
40	820.6			İ	I			_	
41 _	819.6				I		l	1	
42	818.6								
WATER	LEVEL OBS	ERVATIONS:	ADDITIONA				-U- J-W		
	ring drilling:	None Observed		-No ground: upon compl		untered W	ille drillin	gor	
	completion:	None Observed							
Di	epth/Delay: Ceved at:	NA 12+ feet (Fi .848.6+)							
	Caved at: 12± feet (EL 848.6±)								



Caved at: 7.3± feet (EL 862.8±)

SOIL BORING LOG: B-2

midwest engineering services, inc.

Project:

TID #5 Improvements

Project No.: 4-73027

Location:

Prescott, Wisconsin

Drilled by: Joe Black

Drill Date: March 8, 2007

DEP	TH/EL.	VISUAL SOIL CLASSIFICATION	SAMPLE	N	Qp	Qu	мс	REMAR
(f	eet)	GROUND SURFACE ELEVATION: 870.1	NO.	(bpf)	(tsf)	(tsf)	(%)	
٦,	869.1	0-10": Dark brown SILT, with clay, trace sand and organics (TOPSOIL)	1-AU				5.	j
2]	888.1	10-18": Dark brown SILT, little clay, trace sand, damp					ļ	l
, 7	867.1			 		 	<u> </u>	l
. =	866.1		2-SS	2		1	5	
_ ' ᅴ	865.1	Orangish brown silty SAND, damp					,	1
~	-	•	0.00	4	i	t	. 7	1
6 —	864.1		3-55	4	<u> </u>	<u> </u>	· '	
7 →	863.1			<u> </u>	<u> </u>		<u> </u>	İ
ᆥᅴ	862.1		4-88	53		•		
9 _	861.1						<u> </u>	
∘	860.1	•				<u> </u>	<u> </u>	ĺ
11 _	859.1	Tan weathered SANDSTONE	5-SS	94			ŀ	
12	858.1				 			
13	857.1							
,,,,	856.1							
₅ "ૅ╡	855.1				l			
			6-SS \	50/3"		·	7	
16	854.1							
17	853.1	·						
18	852.1	END OF BORING @ 16± FEET						
19 _	851.1	(Auger refusal at 16 feet due to sandstone)						
·	850.1							
21 _	849.1							
22	848.1							
23	847.1							
24	846,1							
5 7	845.1							
28 —	844.1							
27	843.1					l		
28 —	842.1							
29	841.1					1		
	840.1			1				
31	839,1		1				1	
32 _	838.1					•		
33	837.1		ı					
34	836.1		l				I	
, "¬	835.1			İ				
	834.1			l				
36				l				
37	833.1		I	ļ		l		
38 —	832.1				ĺ		l	
39 —	831.1	1		i		1		
` —1	830.1		1		1	ı		
41 📑	829.1	1			I	I	I	
42	828.1			1			1	
WATER	LEVEL OBS	ERVATIONS:	ADDITIONA					
	ring drilling:	None Observed		No ground		untered w	nile drillir	g or
	completion:	None Observed	•	apon compi	540II.			
De	epth/Delay:	NA .						



midwest engineering services, inc.

Project: Location: TID #5 improvements

Prescott, Wisconsin

Project No.: 4-73027 Drill Date: March 8, 2007

Drilled by: Joe Black

DEP	TH/EL.	VISUAL SOIL CLASSIFICATION	SAMPLE	N	Qр	Qu	МС	DENVOYO
ı	leet)	GROUND SURFACE ELEVATION: 875.5	NO.	(bpf)	(tsf)	(tsf)	(%)	REMARKS
, -	874.5	0-12": Dark brown SILT, with clay, trace sand and organics (TOPSOIL)	1-AU					
2 -	873.5	Brown sandy SILT, trace clay, damp	1-20		1	İ	l	Ì
]]]	872.5						-	·
	871.5	Orangish brown silty SAND, damp	2-SS	3	1	l	6	
اءِ ⁺ ≒	870.5	Usangian blown any SAND, damp						٠
		5.8-6.2': Brown clayey SAND, moist	3-SS	36			 	_
§ –	869.5	6.2-6.5': Tan weathered SANDSTONE	<i>-</i> 200	30	<u> </u>			-
′⊣	868.5				l		1	-
8 –	867.5	END OF BORING @ 6.5± FEET			ĺ	•	l	-
9 —	866.5	(Auger refusal at 6.5 feet due to sandstone)						-
10	865.5							
11 _	864.5				<u>'</u>			-
12_	863,5							-
13	862.5							-
14.⊐	861.5	:						_
15	860.5	,						_
16_	859.5	: _.						_
17_	858.5							_
18_	857.5							_
19_	856.5							
20 -	855.5							
21_	854.5							
22	853,5							٦
23	852.5							-
	851.5							7
25	850.5						l	1
								-
26	849,5							1
27一]	848.5	•					I	
28 -	^{847.5} —]		I	1			ı	-
29 —	846.5					1	l	-
30	845.5		1				I	
31 —	844.5			· ·		1		4
32	843.5			1	-			4
33	842.5			I		-		4
34	841.5		I	I	I			-1
35	840.5			į	- 1	j		_
36	839,5		ł	I	I	1		4
37	838.5		1	l	l	[4
38	837.5		1	I	1	1		4
39 _	836.5			l	İ	1	ĺ	_
40	835.5		1	I		I		_]
41	834.5	!	i	l		I	ı	
42 7	833.5							1
WATER	LEVEL OBSE	RVATIONS:	ADDITIONA					
Duri	ing drilling:	None Observed		No groundy		untered w	hile drillin	gor
	•	None Observed	ŧ	pon compl	ellon.			#
De		NA .						
		3.3± feet (EL 872.2±)						

midwest engineering services, inc.

SOIL BORING LOG: B-4

Project: Location: TID #5 Improvements

Prescott, Wisconsin

Project No.: 4-73027
Drill Date: March 8, 2007
Drilled by: Joe Black

	TH/EL. eet)	VISUAL SOIL CLASSIFICATION GROUND SURFACE ELEVATION: 876.2	SAMPLE NO.	N (bpf)	Qp (tsf)	Qu (tsf)	MC (%)	REMAR
, .	875.2	0-15": Dark brown SILT, with clay, little organics, trace sand (TOPSOIL)	1-AU					
2 7	874.2		1-20					
; ;	873.2						-	ł
ĬĦ	872.2	Orangish brown silly SAND, damp	2-SS	4		<u> </u>	6	
, '⊣	871.2	Orangan Brown and Orano, comp						1
	870.2		3-55	36				
• –	869.2					 	 	ł
∵∃	_							
<u>"</u> =	868.2 867.2	Tan weathered SANDSTONE	4-SS	50/1"		ĺ	İ	
, "⊣	866.2		√ 5-SS \	/ 50/1" \				1
			/ 	'				
"∃	865.2							
12	864.2	END OF BORING @ 10.1± FEET	l	1				
13	863.2	(Auger refusal at 10.1 feet due to sandstone)	İ					
14-	862.2							
<u>'</u>	861.2							
16	860.2	·						
17-]	859.2							
18 —	858.2			i i				ĺ
19 —	857.2							
	856.2							
21	855.2						·	
22	854.2	(
23 —	853.2							
24	852.2							
·	851.2							
26 _	850,2							
27	849.2							
28 _	848,2							
29 _	847.2							
	846.2							
31	845.2							
32_	844.2				j			
33 📑	843.2							
34	842.2							
	841.2							
36	840.2							
37	839.2			l	İ	1		
38]	838.2					·]		
39	837.2							
\exists	836.2						ļ	
41	835,2			ļ				
42 -	834.2			<u>_</u>				
VATER		ERVATIONS:	ADDITIONAL COMMENTS:					
	ring drilling:	None Observed		-No ground: upon compl		ountered w	nile drillir	ng or
	completion:	None Observed		المانانى ،،بەر				
De	epth/Delay: Caved at:	NA 4.2± feet (EL 872.0±)						



Project: Location: TID #5 Improvements

Prescott, Wisconsin

Project No.: 4-73027

Drill Date: March 8, 2007 Drilled by: Joe Black

DE	PTH/EL.	VISUAL SOIL CLASSIFICATION	SAMPLE N Qp Qu MC		REMARKS			
	(feet)	GROUND SURFACE ELEVATION: 888.2	NO.	(bpf)	(tsf)	(tsf)	(%)	REMARKS
1_	887.2	0-21": Dark brown SILT, with clay, little organics, trace sand (TOPSOIL)	1-AU					
2_	886.2	David Cili T. I'llia and and along david						
3 _	885.2	Brown SILT, little sand and clay, damp					<u> </u>	
4	884,2	Brown sandy SILT, trace clay, damp	2-SS	6			12	
5	883.2							<u> </u>
6	882.2	Daniel Col AV moint	3-88	15			17	
7 -	881.2	Brown sandy CLAY, moist						
	880.2							
, -	879.2	T	4-SS	50/5"				
10	878.2	Tan weathered SANDSTONE						
11_	877.2		5-SS	50/4"				
12	876.2							
13	875.2							٦
14	874.2		∕ 6-SS \	/ _{50/1"} \				٦
15 -	873.2		1					
	1 -							
16	872.2	END OF BORING @ 14.1± FEET				·		-
17_	871.2	(Auger refusal at 14.1 feet due to sandstone)						-
18	870.2	,					1	-
19	869.2					l	l	4
20	868.2							-
21	867.2							-
22_	866.2			l			1	-
23	865.2					ı	ı	-
24	864.2_					l	l	-
25	863.2			1	Ì	l	ł	_
26	862.2				l	I	I	4
27_	861.2			•	Ì		1	4
28_	860.2			İ	I	I	- 1	4
29	859.2			į	- 1		I	4
30	858.2		ĺ			1	I	_
31	857.2		ĺ	l		.	I	4
32	856.2			1	ļ	ı		4
33 _	855.2	İ		l	- 1	l		4
34	854.2_			I			1	4
35	853.2			l				_
36_	852.2			ł		l	į	1
37	851.2			1	ļ			4
38	850.2		ł			l		ال
39 📑	849.2			1	1	ļ	I	
40	848.2	·		1	1		l	_]
41	847.2			l		1		
42	846.2							
	LEVEL OBS	ERVATIONS:	ADDITIONAL COMMENTS:					
Du	uring drilling:	None Observed		No groundy		intered wi	nile drilling	gor
	completion:	None Observed	U	pon comple	euon,			
	Depth/Delay:	NA						
	Caved at:	6.7± feet (EL 881.5±)						



idwest engineering services, inc.

Project:

TID #5 Improvements Prescott, Wisconsin

Location:

Project No.: 4-73027
Drill Date: March 12, 2007
Drilled by: Joe Black

11	PTH/EL.	VISUAL SOIL CLASSIFICATION	SAMPLE	N	Qp	Qu	МС	REMARKS
(feet)	GROUND SURFACE ELEVATION: 907.4	NO.	(bpf)	(tsf)	(tsf)	(%)	
1 -	906.4	0-18": Dark brown SILT, with clay, little organics, trace sand (TOPSOIL)	1-AU				ŀ	-
2	905.4	Brown SILT, little clay, trace sand, moist]				ļ	-
₃ _	904.4		2-SS	7			13	-
4 4	903.4	Brown SILT, little sand, trace clay, damp			<u> </u>	 	L.º	_
5	902.4						<u> </u>	_
6 _	901.4		3-88	13			-10	
7 _	900,4	Brown SAND, little slit and clay, trace gravel, moist						
₀ _	899.4			- 40			1 6	_
, ∃	898.4_	Yellowish brown SAND, with interbedded clay seams, moist	4-88	12			10	
10	897.4	, , , , , , , , , , , , , , , , , , , ,						
11	896.4		5-88	7			12	
12 -	895.4	Light brown weathered SANDSTONE	/ 6-SS \	/50/0.5°\			7.	
13	894.4	Light bloth recursed of the order	/ 3.00 \	7 00/0.0				
14	893.4	END OF BORING @ 12.6± FEET					1 1	
15	892.4	(Auger refusal at 12.6 feet due to sandstone)						
16	891.4	(Auger relusar at 12.0 reet due (0 sanusture)			i i		<i>,</i> ·	
17]	890.4							1
18	889.4							1
19	888.4						.	1
20	887.4						.]	1
21	886.4					- 1		
22	885.4						. [
23	884.4					I		-
24	883.4			I				-
25 24	882.4		1	l	1	ı		1
	881,4			1				
26					1	l		-
27	880.4		l		1			1
28	879.4					I	I	1
30 29	878.4		l	1	ľ	- 1	ı	- 1
	877.4		1	- 1		- 1	- 1	ᅦ
31 -	876.4		ĺ	l	1			4
32	875.4			1	1		l	-
33	874.4		l				.	4
2 34 →	873.4				1		. 1	-
35	872.4		l		- 1			-
36	871.4			1	1	ĺ		4
37_	870.4			I	1	1	1	4
38 _	869.4				- 1	- [İ	4
39_	868.4		Ī			1		4
40	867.4				1		1	
41-7	855.4		1]		ľ		4
42 7	865.4	TNATIONS.	ADDITO	1 001212	ITE.			
	LEVEL OBSE	RVATIONS: None Observed	ADDITIONAL	L COMMEN No groundw		intered wh	ile drilling	a or
		None Observed		pon comple		>= 111		
		NA .						#
	Caved at:	10± feet (EL 897.4±)						



TID #5 improvements

Project No.: 4-73027
Drill Date: March 12, 2007
Drilled by: Joe Black Project: Location: Prescott, Wisconsin

II	TH/EL.	VISUAL SOIL CLASSIFICATION GROUND SURFACE ELEVATION: 912.4	SAMPLE NO.	N (bpf)	Qp (tsf)	Qu (tsf)	MC (%)	REMARKS
				(4,7,7)	(44.7)	\ <u>\</u>	 	
∥ ¹⊣	911.4	0-15": Dark brown SiLT, little clay, trace sand and organics (TOPSOIL)	1-AU			l	1	-
2 -	910.4							
3 —	909.4		2-88	9	•	l	14	-
∥ ⁴⊣	908.4	Brown sandy SILT, trace to little clay, damp		-		\vdash	 	-
5	907.4					 		
6 →	906.4		3-SS	11			14	-
7-7	905.4							-
8 =	904.4		4-55	18			3	_
9	903.4		+00				L	_
10	902.4							
∥ "_ქ	901.4	White, brown and orange SAND, trace silt, damp	5-SS	19			3	_
12_	900,4	•						
13	899.4							
147	898.4]
15	897.4							
16_	896.4		6-SS	50/4"				
17	895.4	Towns of DANIDOTONIE						1
18	894.4	Tan weathered SANDSTONE	/	/\				1
19"	893.4		/ 7-SS \	/ 50/0.5" \				
20 "	892.4							1
		END OF BORING @ 18.1± FEET				ı		
21	891,4	(Auger refusal at 18.1 feet due to sandstone)						1
22	890.4	,			l	ı		4
23 -	889.4					ĺ		- 1
24 —	888.4	•				1	ı	-
25	887.4			ı	Ì			-
26	886.4					ı	l	4
27	885.4					- 1	ı	-
28 —	884.4				- 1	- 1		4
29	883,4							4
30	882.4			ı	- 1	- 1	1	_
31	881.4	•		l				4
32	880.4			J	ļ	ı		4
33_	879.4		į	I				4
34	878.4	1	l	l	İ	1		4
35	877.4		1	I	l			
36	876.4	1	l	ł	1			
37	875.4	İ	ĺ	I	- 1			
38 =	874.4		l	l	1]
39	873,4			İ		l		1
40	872.4				l			7
41 _	871.4				-	l		
42	870.4			į	I	1		1
		RVATIONS:	ADDITIONA	L COMMEN	ITS:		······································	
		None Observed	-No groundwater encountered while drilling or				g or	
	-	None Observed	ti	pon comple	etion.			
		NA .						
*********************************	Caved at:	14,6± feet (EL 897.8±)			·····			

Project:

TID #5 improvements

Location:

Prescott, Wisconsin

Project No.: 4-73027 Drill Date: March 12, 2007

Drilled by: Joe Black

H	PTH/EL.	VISUAL SOIL CLASSIFICATION	T	SAMPLE	N	Qp	Qu	MC	REMARKS
	(feet)	GROUND SURFACE ELEVATION: 929.4	4	NO.	(bpf)	(tsf)	(tsf)	(%)	
· <u>·</u>	928.4_	0-7": Dark brown SILT, with clay and organics, little sand (TOPSOIL)	1	1-AU		1	1		_
2 -	927.4	- 7-13": Brown clayey SAND, moist	1		l	1	l	l	
, -	926.4	13-30": Orangish brown silty SAND, trace clay, moist	-						-
	925.4	-	' I	2-88	12	1	1	5	-
5 -	924.4		\vdash				1		-
	1		\vdash			-	 		
5-	923.4_			3-88	6			5	-
7 _	922.4	Light brown SAND, with interbedded clay seams, trace slit, damp	Г		i				-
8 _	921.4_			4-88	15			2	_
9	920.4	,	—	. 00		<u> </u>			_
10	919.4		\perp						_
11_	918.4	<u>i</u>	1	5-SS	21			2	
12_	917.4_		\vdash			1			
13	916,4		l			[٦
14 -	915.4								1
15	914.4			ĺ			j j		4
	913.4		十	6-SS	47				
16		Brown SAND, trace silt, damp		<i>y</i> -33	47			2	4
17_	912.4	Brown SAND, trace slit, damp					l l		4
18 -	911.4		j]]	İ	-
19	910.4	Tan weathered SANDSTONE	7 ~	\ I	$\overline{}$		l í		-1
20	909.4		V_{-}	7-55	/ 50/4" \				
21 _	908.4								
22_	907.4	END OF BORING @ 20.4± FEET		l					
23	906.4		1					- 1	
24_	905.4			- 1				1	
25	904.4		l						1
26	903.4							l	
27	902.4		l	- 1				1	1
28	901.4		1						1
					l				-1
29 <u>]</u>	900.4		İ	I		ı			-1
30	899.4				I				-
31	898.4			İ		I	l		-
32_	897.4			I	į		1		4
33 _	896.4				l	I	j	l	4
34_	895.4		l	- 1	1	l	1		4
35	894.4				- 1			- 1	
35	893,4_		l	l	l	l			
37	892.4			-	l]		ı	7
38	891.4				l	1			1
39 7	890.4				l	I			1
40 ³³ 寸	889,4				I		ļ		4
	_				I				-
41 —	888.4			1		- 1		ı	4
42]	887.4 T	:DVATIONS:	A.D.	DUTTONA		<u></u>	L		
	LEVEL OBSE ring drilling:	RVA HONS: None Observed	ΑÜ		COMMENTO COMPANDO COM		untered wh	ile drilling	or
	ompletion:	None Observed			pon comple		,110104 1911		-
		NA NA							
	Caved at:	15± feet (EL 914.4±)							
	on of stealifier						***************************************	-	



midwest engineering services, inc.

Project: Location: TID #5 Improvements

Prescott, Wisconsin

Project No.: 4-73027

Drill Date: March 12, 2007 Drilled by: Joe Black

DEPTH/EL. VISUAL SOIL CLASSIFICATION SAMPLE Qu N Qρ REMARKS GROUND SURFACE ELEVATION: 919.1 (bpf) (tsf) (tsf) (%) 0-13": Dark brown SiLT, with clay and organics, little sand (TOPSOIL) 918.1 1-AU 13-18": Dark brown SILT, little clay, trace sand, moist 917.1 916.1 2-SS 15 18 Brown SILT, with clay, little sand, damp 915.1 914.1 913.1 3-SS 5 16 Orangish brown sandy SILT, little clay, damp 912.1 911.1 **4-SS** 11 10 910.1 909.1 7 27 908.1 5-SS Light brown silty SAND, with day seams, damp 907.1 906.1 905.1 6-55 33 903.1 5 902.1 Brown SAND, with gravel, trace slit, damp 899.1 7-88 29 3 898.1 897.1 896,1 END OF BORING @ 21.5± FEET 895,1 894.1 893.1 892.1 891.1 890.1 889.1 886.1 885.1 883,1 881.1 880.1 879.1 878.1 WATER LEVEL OBSERVATIONS: ADDITIONAL COMMENTS: -No groundwater encountered while drilling or During drilling: None Observed upon completion. None Observed Upon completion: Depth/Delay: NA

15.5± feet (EL 903.6±)

Caved at:



Project: Location: TID #5 Improvements

Prescott, Wisconsin

Project No.: 4-73027 Drill Date: March 5, 2007

Drilled by: Joe Black

1	TH/EL.	VISUAL SOIL CLASSIFICATION GROUND SURFACE ELEVATION: 899.6	SAMPLE NO.	N (bpf)	Qp (tsf)	Qu (tsf)	MC (%)	REMARKS
			110.	(Opi)	(co.)	(131)	(70)	
l ¹⊣	898.6	0-15": Dark brown SILT, with clay and organics, little sand (TOPSOIL)	1-AU			l		
│ ²⊣	897.6	Brown SiLT, with clay, little sand, damp					 	
3-7	896.6		2-SS	10			5	
⁴⊐	895.6						<u> </u>	-
5	894.6	Orangish brown SAND, little clay and gravel, damp	<u> </u>				ļ	_
ᆘ	893.6		3-SS	9			3	_
7 -	892.6		 					_
₀_	891.6		4.00	F0/F1				_
9 -	890.6		4-88	50/5"				_
10	889.6	Brown and tan weathered SANDSTONE						
11 -	888.6	Brown and tan weathered SANDSTONE	/# BB	50/1"				
12	887.6		5-SS	/ 50/1				
	886.6							_
13	885.6							_
15 -	884.6	END OF BORING @ 11.6± FEET					, i	-
		(Auger refusal at 11.6 feet due to sandstone)						_
16_	883.6						i	-
17	882,6				i	İ		-
18	881.6					ĺ		4
19	880.6		ļ					-
20	879.6		1 1					
21 _	878.6		1 1					4
22_	877.6			1				-
23	876.6				- 1	- 1		-
24	875.6] [1	ı	· [4
25	874.6					.		_
26	873,6				ı	1	1	
27	872.6		l 1	I	.	l	l	_
28 _	871.6			- 1			ı	_
29	870.6	•		l	i		l	
30	869.6]		1	l	1	
31 _	868.6			l		l	l	
32	857.6			-1	- 1	l	I	7
33 =	866.6					I	1	
34	865.6	×		l		I		1
35	864.6			ĺ	1	l		1
		•		l	- 1			
35 -	863.6				l	ı	ĺ	1
37	862.6				l			-
38 —]	861.6				I		- 1	1
39 -	860.6			1	-	1]	4
40	859.6					1		ᅰ
41 -	858.6				l	1		-
42 7	857.6	DV4 TIONO.	ADDITIONS	COLLECT				
	LEVEL OBSE		ADDITIONA	L COMMEN No groundy		intered wi	nile drilling	or
		None Observed None Observed		pon comple		111		
	•	NA NA						
50		4.3± feet (EL 895.3±)						



midwest engineering services, inc.

Project: Location: TID #5 Improvements

Prescott, Wisconsin

Project No.: 4-73027

Drill Date: March 9, 2007 Drilled by: Joe Black

ii	PTH/EL.	VISUAL SOIL CLASSIFICATION	SAMPLE	N	Qp	Qu	MC	REMARKS
	(feet)	GROUND SURFACE ELEVATION: 883.2	NO.	(bpf)	(tsf)	(tsf)	(%)	
1 1	882.2_	0-19": Dark brown SILT, little clay and organics, trace sand (TOPSOIL)	1-AU		1			
2_	881.2_	Dark brown SILT, little clay, trace sand, damp			ļ			
3 _	880,2_				<u> </u>		45	
4_	879.2	Light brown sandy SiLT, trace clay, damp	2-SS	6			15	
5	878.2							_
6 _	877.2		3-SS	5	l		7	
7_	876.2	Brown clayey SAND, little gravel, moist				<u> </u>		
8_	875.2	Light brown silty SAND, little sandstone fragments, damp	1	40			40	
9	874.2	Light bronn day of this, indicates to haghinate, camp	4-88	12			10	_
10	873.2	Tan to light gray weathered SANDSTONE	 					_
11_	872.2	Tan to agric gray violation of or the original and the same of the original and the same of the original and the same of the original and the same of the original and the same of the original and the same of the original and the same of the original and the same of the original and the original	5-SS	50/1"				
12_	871.2	END OF BORING @ 11.1± FEET			,			
13 _	870.2	(Auger refusal at 11.1 feet due to sandstone)						_
14_	869.2	(agos rosadar at 11.1 foot data to danastano)						
15	868.2							_
16	867.2							
17	866.2	·						_
18	865.2							
19_	864.2				ĺ			
20	863.2							_
21	862,2							
22]	861.2							_
23	860.2							
24 -	859.2							
25	858.2							_
26_	857.2	-				·	I	_
27	856,2					Į.	•	_
28	855.2		1 1					_
29	854.2			l		ı		
30	853.2				l			
31_	852.2			l			- 1	_
32	851.2				İ	1		
33	850,2				ł			
34	849.2			l	1	j		4
35	848.2			ŀ	I	l	1	
36	847.2_				l	ı		4
37	846.2		1	ŀ	l	I	- 1	4
38_	845.2_					- 1	I	4
39	844.2			1				4
40	843.2					1	ı	_
41_	842.2							
42	841.2			<u>_</u> 1				
	LEVEL OBSE		ADDITIONA	L COMMEN No grounds		unfored ····	سالانجام والد	. or
	ring drilling: completion:	None Observed None Observed		no grounav		mireied Mi	me ulmin	y U1
	completion: epth/Delay:	NA NA						
	Caved at:	5.3± feet (EL 877.9±)						1



Project:

Location:

SOIL BORING LOG: B-12

Project No.: 4-73027 Drill Date: March 9, 2007 TID #5 Improvements Prescott, Wisconsin Drilled by: Joe Black

	TIVE!	T VICTAL COLL OF ACCIPICATION	SAMPLE	N	Qp	Qu	MC	
11	PTH/EL. (feet)	VISUAL SOIL CLASSIFICATION GROUND SURFACE ELEVATION: 864.8	NO.	(bpf)	(tsf)	(tsf)	(%)	REMARKS
		O-12": Dark brown SILT, little sand and clay, trace organics (TOPSOIL)	NO.	(DPI)	(131)	(131)	(/0/	
1_	863,8	10-12. Dark blown Sic.1, little sailt and clay, trace organics (10-30:L)	1-AU	l		1	l	-
2_	862.8_	1			├	 	ļ	-
3	861.8_	Dark brown SILT, little sand, trace clay, damp	2-SS	4			13	-
4_	860.8		2-00		ļ		L."	_
5	859.8			1		<u></u>		
6_	858,8		3-SS	4			12	
7 -	857.8			 	 			
8 -	856.8	Brown SiLT, little sand and clay, damp		 	 			1
9 -	855,8		4-SS	5	İ.		4	Ī
10 -	854.8 -							1
			5-SS	24			_ 1	_
11_	853,8	Light brown SAND, trace silt and gravel, damp	5-55	24			- '	-
12_	852.8							-
13	851.8		1	l				-
14 🗇	850.8							-
15	849.8							_
16_	848.8	Tan SAND, with silt and sandstone fragments, damp	6-SS	23			7	-
17	847.8							_
18_	846.8							_
19	845.8							
20 -	844.8							
21_	843.8	Tan weathered SANDSTONE	7-SS	50/1.5"				
22	842.8							
23	841.8							٦
		END OF BORING @ 21.5± FEET						1
24 <u> </u>	840.8 839.8 -							1
						- 1	1	-
26_	838.8					•	- 1	
27	837.8					l	l	4
28	836.8							-
29	835.8					1	- 1	4
30	834.8					ľ	.	_
31 _	833.8					- 1	l	4
32	832.8			l		1		
33	831.8					l	į	
34	830.8			I	- 1	.[I]
35	829.8				1	1		. 7
36	828.8				l	1		
7]	I		1
37	827,8		, i	1	l		1	1
38∃	826.8				- 1		l	4
39 —	825.8]		l	1	İ	4
40	824.8						Į	_
41	823.8	Ì			İ	l		4
42 -	822.8			1				
	LEVEL OBSE	3	ADDITIONA			untarad · · ·	-الله مالة -العام مالة	
	ring drilling:	None Observed		No ground: upon compl		unterea Wi	nie anilin	g or
•	completion:	None Observed	,					
D	epth/Delay: Caved at:	NA 11± feet (EL 853.8±)						
	Jayou at.	111 /BSI (LL 000:01)						



Project:

TID #5 improvements

Location:

Caved at: 4± feet (EL 863.9±)

Prescott, Wisconsin

Project No.: 4-73027 Drill Date: March 9, 2007 Drilled by: Joe Black

	TH/EL.	VISUAL SOIL CLASSIFICATION	SAMPL		Qp (4-0	Qu	MC	REMARKS
(feet)	GROUND SURFACE ELEVATION: 867.9	NO.	(bpf)	(tsf)	(tsf)	(%)	
1 _	866.9	0-10": Brown SILT, with clay and organics, trace sand (TOPSOIL)	1-AU		1		l]
2_	865,9_	Brown SILT, little sand and clay, moist				<u> </u>	<u> </u>	
3 _	864.9				 	 	i -	1
4	863,9	Brown silty SAND, damp	2-SS	3	<u> </u>	<u> </u>	6	1.
5	862,9							_
8 7	861.9	Brown SAND, little silt and gravel, damp	3-88	8			3	_
-, =	860.9					 	- 1	·
: 4	859.9	Tan weathered SANDSTONE	4-SS	50/3"			<u> </u>	
្នុំដ	858.9		İ	l		ĺ	ĺ	
。"ヸ	857.9	END OF BORING @ 7.8± FEET	ļ	-		1		
		(Auger refusal at 7.8 feet due to sandstone)					.:	-
11 -	856.9							
12	855.9							
13	854.9		I	i	İ	ĺ		
14 _	853,9		1		· ·			
5	852.9		1					_
16_	851,9							
17	850,9		Î					
18_	849.9							
19_	848.9		1					
\vdash	847.9			l			·	
21	846.9							
22	845.9		Ì	l				•
23	844.9		1					•
	843.9		l					-
24	842.9							-
	-							-
26	841.9							-
27	840.9						·	-
28	839.9		1				·	-
29 _	838.9						.	-
' —[837.9		j					-
31	836.9		İ			l	I	-
32	835,9		1					_
33 📑	834.9						٠.	_
34	833.9_					l		
;	832.9						I	
36	831.9					i	I	
37	830.9				ĺ		I	_
38	829.9					ı	. [7
39	828.9		1				.	1
, "=	827.9		1		I	I		٦
	_			1 1		- 1		
41 —	825.9							-
42 7	825.9 T	ERVATIONS:	ADDITIO	NAL COMME	NTS:	L		
	ing drilling:	None Observed	755,,,,,	-No ground		untered w	hile drillin	g or
	completion:	None Observed		upon comp				
	epth/Delay:	NA NA						
	Deputitionary, IVA							



Project: Location: TID #5 Improvements

Prescott, Wisconsin

Project No.: 4-73027

Drill Date: March 9, 2007 Drilled by: Joe Black

ll .	TH/EL.	VISUAL SOIL CLASSIFICATION	SAMPLE	N	Qp	Qu	MC	REMARKS
(1	feet)	GROUND SURFACE ELEVATION: 866.2	NO.	(bpf)	(tsf)	(tsf)	(%)	
1寸	865.2	0-14": Dark brown SILT, little sand, trace clay and organics (TOPSOIL)	1-AU					-
2 -	864.2 863.2							-
	862.2	Dark brown SILT, trace sand and clay, damp	2-88	6	<u> </u>	<u> </u>	13	
5	861.2							_
6 _	860.2		3-SS	3		İ	13	_
7-	859.2	Brown SILT, little sand and clay, damp						-
• -[858.2	Biothi Gig I, indo dana and day, damp	4-SS	7			9	-
<u>"</u> ° -]	857.2	Brown SAND, little silt, trace day and gravel, moist						7
10	856.2		5-SS	25			2	
11	855.2 854.2	Light brown SAND, trace silt and gravel, damp	0-00				-	1
13 -	853.2]
14	852.2							_
15	851.2	Grayish brown silty CLAY, trace sand, moist						_
16	850.2_		6-SS	5	<0.25		18	-
17	849,2							-
18	848.2							-
20 -	847.2 846.2 -							-
21	845.2	Orangish brown clayey SAND, with gravel, moist	7-SS	9			10	_
22	844.2							
23	843.2	END OF BORING @ 21.5± FEET						_
24	842.2	2.15 01 201.11.10 (2.11.12.1.22.1						_
25	841.2							-
26	840.2						l	4
27 —	839.2						ļ	-1
28	838.2		Ī			ı		1
30 29	837.2 836.2						3	1
31 _	835.2							
32	834.2]
33 📑	833,2							4
34_	832.2							4
35	831.2					I		-
36 —	830.2				l	ĺ	l	4
37	829.2	1						-
38 →	828.2 827.2	T T T T T T T T T T T T T T T T T T T			Ì	l		1
40 39	826.2						I	
41	825,2					1		
42]	824.2		1					
		ERVATIONS:	ADDITIONA	L COMME! No ground		untered w	hile drillin	a or
	ing drilling: completion:	None Observed None Observed		ipon compl		antoreu W	c uma	5 51
•	epth/Delay:	NA NA						
	Caved at:	13.6± feet (EL 852.6±)						



Project: Location: TID #5 Improvements

Prescott, Wisconsin

Project No.: 4-73027 Drill Date: March 9, 2007

Drilled by: Joe Black

11	PTH/EL.	VISUAL SOIL CLASSIFICATION	SAMPLE	N	Qp (c. 0	Qu	MC	REMARKS	
 	(feet)	GROUND SURFACE ELEVATION: 870.1	NO.	(bpf)	(tsf)	(tsf)	(%)		
1	869.1	0-15": Dark brown SILT, with clay, trace sand and organics (TOPSOIL)	1-AU			l	1	-	
2_	868.1_	Brown SILT, little sand and clay, moist	ļ	 	<u> </u>	L			
з	867.1		2-SS	6			11	-	
4_	866.1	Brown silty SAND, damp	2-30	<u> </u>	<u></u>			-	
5	865.1			<u> </u>				_	
6	864.1		3-SS	13			6		
7_	863.1	Light brown SAND, with clay cells, moist	<u> </u>		-				
8 -	862.1		-						
9 -	861.1	Tan weathered SANDSTONE	4-SS	50/5.5"					
10	860.1	Tall Weathered GANDSTONE.							
11	859.1		5-SS	50/5"					
12_	858.1								
13	857.1								
14 -	856.1								
15 -	855.1	END OF BORING @ 12.0± FEET						1	
-	1	(Auger refusal at 12 feet due to sandstone)						-	
16	854.1							- 1	
17	853,1							-	
18	852.1							-	
19_	851.1							-	
20	850.1							-	
21 _	849.1						I		
22_	848.1				I		ı	-	
23_	847.1						- 1	4	
24	846.1				i		I	4	
25	845.1					,			
26_	844.1				ı			4	
27	843.1							4	
28	842.1			1	l	- 1	ili di di di di di di di di di di di di di		
29	841.1_			l	ı	- 1	I	4	
30	840.1			ĺ	I	1	1	_	
31	839,1		İ	- 1		ı	1		
32	838.1			1		- 1			
33]	837.1			1		1			
34	836.1			1	I	- 1		7	
35 ~~ =	835.1			1		.]		1	
36	834.1			l			l		
	833.1		l			l	1	1	
37	_					į	1	1	
38 —	832.1				ĺ	- 1	ı	1	
,, ₃9-]	831.1		l			l	1	┪	
40	830.1				l		İ		
41-]	829.1							4	
42 7	828.1 7	TOVATIONS	ADDITIONA	COMMEN	ITC.				
	LEVEL OBSI	ERVATIONS: None Observed		L COMMER No groundy		untered wi	nile drillin	or I	
	completion:	None Observed		pon comple					
	epth/Delay:	NA .						1	
	Caved at: 5.3± feet (EL 864.8±)								



Project No.: 4-73027 Drill Date: March 9, 2007 Drilled by: Joe Black

TID #5 Improvements Project: Location:

Prescott, Wisconsin

DEI	PTH/EL.	VISUAL SOIL CLASSIFICATION	SAMPLE	N	: Qp	Qu	MC	l DEMARKS
II .	(feet)	GROUND SURFACE ELEVATION: 869.8	NO.	(bpf)	(tsf)	(tsf)	(%)	REMARKS
1 -	868.8	0-17": Dark brown SILT, little sand and clay, trace organics (TOPSOIL)	1-AU					_
2 _	867.8	Brown SILT, little sand, trace clay, damp			<u> </u>		 	-
3_	866.8		2-SS	7	i –		14	-
4 _	865.8	Light brown SILT, little sand, trace clay, damp		 		 	<u> </u>	-
5	864.8			1	 		 	_
6	863.8		3-SS	4			8	-
7 _	862.8	Brown clayey SAND, little gravel, moist			<u> </u>			-
8	661.8		4- SS	33				
10 9 -	859.8 859.8							-
11_	858.8	Tan weathered SANDSTONE	5-SS	52				-
12	857.8	·			<u> </u>			
13	856.8	·						
14	855,8			/				
15	854.8		/ 6-SS \	/ 50/1.5" \	<u> </u>		 	
16	853.8	END OF BORING @ 14.7± FEET						-
17_	852.8	(Auger refusal at 14.7 feet due to sandstone)						_
18_	851.8							_
19_	850.8							-
20	849.8							_
21_	848.8							-
22_	847.8	,						-
23	846.8	,						4
24	845.8							1
25	844.8							
26	843.8							4
27 _	842.8							
28 _	841.8				:			4
29 _	840,8							
30	839.8							-
31	838.8							4
32	837.8							- 1
33	836.8					İ	ĺ	1
25 ³⁴ —	835.8				j			-
35	834.8							
36	833.8							1
37	832.8							1
38	831.8						l	1
40 ³⁹	830.8 829.8				1	l	I	1
	828.8			l	1		1	
41	827.8							1
WATER	LEVEL OBS	ERVATIONS:	ADDITIONA	L COMME	NTS:			
Du	ring drilling:	None Observed		No ground		untered w	hile drillin	g or
•	completion:	None Observed	1	upon compl	edon.			
Đ	epth/Delay:	NA 6.84 foot (El. 863.24)						
	Caved at:	6.6± feet (EL 863.2±)						



Project:

TID #5 Improvements Prescott, Wisconsin

Location:

Project No.: 4-73027 Drill Date: March 12, 2007 Drilled by: Joe Black

DEI	PTH/EL.	VISUAL SOIL CLASSIFICATION	SAMPLE	N	Qp	Qu	MC	
11	(feet)	GROUND SURFACE ELEVATION: 902.7	NO.	(bpf)	(tsf)	(tsf)	(%)	REMARKS
1 -	901.7	0-10": Dark brown SILT, with clay and organics, trace sand (TOPSOIL)	1					
2 -	900.7_		1-AU					•
[:-	899.7	Orangish brown SiLT, little sand and clay, damp						
	1 -		2-SS	17			5	-
∦ _ ⁴ −	898.7_ 897.7	Brown clayey SAND, little gravel, damp			 	 	ŧ	-
J			1		<u> </u>	†	4	-
6 –	896.7_	Brown SAND, with gravel, little clay, damp	3-SS	20		<u> </u>		-
7-	895.7						l	-
°-	894.7		4-SS	69				-
9 _	893.7	Tan weathered SANDSTONE	/ 5-SS \	/50/0.5"\		-	ł	
10	892.7		/ 333 /	/	_	<u> </u>		
11_	891.7							-
12_	890,7	END OF BORING @ 10.1± FEET				1		-
13_	889.7	(Auger refusal at 10.1 feet due to sandstone)						-
14_	888,7							-
15	887.7						l i	-
16	886.7							4
17	885.7							- 4
18_	884.7							_
19_	883.7							_
20	882.7							
21	881.7							
22	880.7							
23	879.7							
24	878.7							
25	877.7							
26	876.7					- 1		
27	875.7							1
28	874.7					1		1
29	873.7		1	ı	1			1
30 -	872.7			i		l	- 1	1
				1		l	ł	
31	871.7					ı	l	1
32	870.7					I	ļ	1
33	869.7				1	I		4
34 35	868.7			1	I	l		4
	867.7		- [ı		I		-
36 _	866.7		1	- 1	I	l	į	4
37 —	865.7		l		I	I		-
38 —	884,7			1	I	I		4
39 —	863.7			-			1	4
40	862.7					1	1	_
41 🗖	861.7_							4
42 1	860,7	1		1 001:::::	170.			
		ERVATIONS:	ADDITIONA	L COMMEN No groundy		untered wi	hile drillin	ı or
	ring drilling: completion:	None Observed None Observed		pon comple			e umini	,
	epth/Delay:	NA NA						ŀ
Caved at: 6.1± feet (EL 896.6±)								



midwest engineering services, inc.

Project: Location:

TID #5 Improvements

Prescott, Wisconsin

Project No.: 4-73027 Drill Date: March 8, 2007

Drilled by: Joe Black

DE	PTH/EL.	VISUAL SOIL CLASSIFICATION	SAMPLE	N	Qp	Qu	MC	
	(feet)	GROUND SURFACE ELEVATION: 896.1	NO.	(bpf)	(tsf)	(tsf)	(%)	REMARKS
1	895.1	0-10": Brown slity, clayey SAND, with sandstone fragments (FILL)						
]	894.1	Brown SiLT, little clay and sand, damp	1-AU	1	1			-
	7 -	DIOWIT OIL!, III. day and saild, dairip						-
3 -	893.1		2-88	50/6"		ļ		-
_ 4 -	892.1							-
5	891.1	Town week and CANDSTONE	_		-	 		_
6_	890.1	Tan weathered SANDSTONE	3-SS	50/4"				-
7 _	889.1							4
8_	888.1		4-88	50/5"				_
9	887.1							_
10	886.1		5-SS \	50/5"				
11_	885.1							
12_	884.1	END OF BORING @ 10.1± FEET						
13 -	883.1	_						1
14 -	882.1	(Auger refusal at 10.1 feet due to sandstone)					1	٦
15	881.1						l	1
16_	880.1							
	_							1
17_	879.1		1				ı	1
18	878.1		[ĺ	l	-
19	877.1						ı	-
20	876.1							_
21_	875.1					l	- 1	4
22_	874.1					- [1	4
23_	873.1			Ì		i	1	4
24	872.1			l		- 1	1	- 4
25	871.1		1 1	l			ļ	
26_	870.1			- 1	1		1	
27	869.1			I			- 1][
28	868.1			I	I		- 1	
29 🗔	867.1		1 1	1				1
30 -	866.1			I	- 1	- 1	1	
31	865.1		1 1		- 1	- 1	I	
ı	864.1				İ	1	- 1	1
32	863.1					- 1		-
33						1		\dashv
⋒ अ∃	862.1		1 1				- 1	4
35	861.1		1 1	1				-
36	860.1			ļ	l	Ĭ		-
37	859.1	•		I				4
38_	858.1			ľ		- 1	l	4
39	857.1			- 1		1	1	4
40	856.1			1	- 1	I		_
41_	855.1			- 1	j]	- 1	4
42 -	854.1			L				
	LEVEL OBSE		ADDITIONA					
		None Observed		No groundw pon comple		intered wh	ile drilling	or
		None Observed	·	pon withle	andii.			
D		NA 5.4± feet (EL 890.7±)						
	Caved at:	U.4I (EE (EL 03U./I)						



Project: Location: TID #5 Improvements

Prescott, Wisconsin

Project No.: 4-73027

Drill Date: March 8, 2007

Drilled by: Joe Black

? {	PTH/EL.	VISUAL SOIL CLASSIFICATION GROUND SURFACE ELEVATION: 891.1	SAMPLE NO.	N (bpf)	Qp (tsf)	Qu (tsf)	MC (%)	REMARKS
		0-10": Brown silty, clayey SAND, with sandstone fragments (FILL)		1-1-1/			\''',	
'⊣	890.1	o io i pioni anni i dan anni anni anni anni anni a	1-AU		l			
l ² →	889,1	Brown SILT, little clay and sand, damp						
『 그	888.1		2-88	38			5	
4-7	887.1	Yellowish brown SAND, damp						-
5	886.1			 	 	<u> </u>		
6 _7	885.1		3-SS	67				-
7-	884.1							-
╽゜┇┛	983.1		4-SS	79				-
l °⊐	882.1	Tan weathered SANDSTONE						-
10	881.1		ļ					-
11	880.1_		5-SS	50/4.5		,		_
12_	879.1			$\overline{}$		-		_
13_	878.1		6-SS	/ 50/1" \				
14	B77.1_							
15	876.1	END OF BORING @ 13.1± FEET						
16	875.1	(Auger refusal at 13.1 feet due to sandstone)						
17	874.1							
18	873.1							_
19 -	872.1		1 1					
20 -	871.1							1
	870.1							-
21	_		1				ı	1
22	869.1						1	7
23-]	868.1		1 1	l		1	I	-
24	867.1		1 1					-
25	866.1]]	ı		l	ı	
26	865,1					1	I	-
27 —	864.1					I	1	4
28 —	863.1		1 1			1		-
29 —	862.1		1 1			1	- 1	4
30	861.1							
31	860.1		1. 1	- 1		l		4
32	859.1			I	l	1		-
33 📑	858.1			I		- 1	l	4
34	857.1			l	i		I	4
35	856.1				İ	j	l	_
36	855.1				I	l	l	4
37_	854.1					i		4
38	853.1			1		l		_
39	852.1				l	I		
40	851.1				l	ł		
41 _	850.1			I	l	1	1	
42 7	849.1							
WATER	LEVEL OBSE	RVATIONS:	ADDITIONA					
	ring drilling:	None Observed		No groundy pon comple		untered wi	nile drillin	gor
	completion:	None Observed	1	ipas windi	-uui.			
De	epth/Delay: Caved at:	NA 7± feet (EL 884.1±)						
		ri leti (EL 004. ii)						



TID #5 Improvements

Prescott, Wisconsin

Project:

Location:

SOIL BORING LOG: B-20

Project No.: 4-73027
Drill Date: March 8, 2007
Drilled by: Joe Black

DEP	TH/EL.	VISUAL SOIL CLASSIFICATION	SAMPLE	N	Qp	Qu	МС	lenve.
	eet)	GROUND SURFACE ELEVATION: 893.4	NO.	(bpf)	(tsf)	(tsf)	(%)	REMARK
, -	892.4	0-19": Brown silty, clayey SAND, with sandstone fragments (FILL)						
_'∃	_	0-19 . Blown sitty, clayey or not, with salidatone magnitude (1722)	1-AU		l	l	l	l
²-J	891.4				 _ _			1
3 —	890.4		2-SS	50/1.5"				l
4 -	889.4	Tan weathered SANDSTONE			-	 	 	ł
5	888.4							
6	887.4		3-SS	65] ,	1	l
7 년	886.4							1
8 -	885.4							
F.	884.4		4-SS \	/ 50/1" \			<u> </u>	j
10	883.4							
	882.4	END OF BORING @ 9.1± FEET					l	•
11-		(Auger refusal at 9.1 feet due to sandstone)						
12	881.4	,	ł				l	
13 —	880.4	1				ĺ	l	l .
14	879.4		1					
15	878.4		1					-
16_	877.4							
17_	876.4	1						
18	875.4							
19	874.4							
20 7	873.4							
21 —	872.4							'
22 _	871.4		1 1					
23 —	870.4							
24 —	869.4							
25	868.4							_
26	867.4							
27	866.4							
28	865.4							
29	864.4		1 1	ı		l		
	863.4							
	862.4						- 1	-
31 —			1 1			l		•
32 <u> </u>	861.4		1		ı			•
33	860.4					ı	ı	•
34 🖳	859.4			ì			- 1	-
5	858.4				ı		1	_
36	857.4			1		I		-
37_	856.4			į	l	1	i	
38	855.4		1 1		l	I		
39	854.4		[l	l	
. " =	853.4			İ		1	I	•
	852.4		1 1		l	l	ı	_
41 -				I		1	l	
42 T	851.4 T	ERVATIONS:	ADDITIONA	I COMME	NTS:		1	<u> </u>
	LEVEL OBSI ing drilling:	None Observed		No ground		untered w	hile drillin	g or
	ompletion:	None Observed		pon compl				-
	ompletion. epth/Delay:	NA NA	1					
	Caved at:	4.5± feet (EL 888.9±)	1					



midwest engineering services, inc.

Project: Location: TID #5 Improvements

Prescott, Wisconsin

Project No.: 4-73027 Drill Date: March 8, 2007

Drilled by: Joe Black

DE	PTH/EL.	VISUAL SOIL CLASSIFICATION	SAMPLE	N	Qp	Qu	MC	l .
ii	(feet)	GROUND SURFACE ELEVATION: 881.2	NO.	(bpf)	(tsf)	(tsf)	(%)	REMARKS
1 -	880.2	0-6": Brown SILT, mixed with dark brown SILT, little clay, trace sand (FILL	·	1	<u> </u>	<u> </u>	` <u>``</u>	
	879.2	6-20": Brown SILT, little sand, trace clay, damp	1-AU			ŀ		-
2 -								-
3 -	878.2		2-SS	50/2.5"				-
5 1-	877.2 876.2			 				-
								_
▍▝ᅴ	875.2	Tan weathered SANDSTONE	3-88	50/4"		<u> </u>		-
⋴	874.2		L	<u> </u>				-
▍゜▘┤	873.2		4-SS	50/1"				-
. . °∃	872.2		√ 5-SS \	/ 50/1" \		\vdash		-
10—	871.2		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	/ 55.1		ļi		
"⊣	870.2					·		-
12 —	869.2	END OF BORING @ 10.1± FEET						-
13	868.2	(Auger refusal at 10.1 feet due to sandstone)						4
14	867.2_							4
15	866.2							E07.0
16_	865,2							4
17_	864.2						I	4
18	863.2_					j		4
19	862.2							4
20	861.2						l	_
21	860.2_				· I		1	_
22_	859.2				1	ŀ	ĺ	J
23	858.2	į				.	1]
24	857.2				1		I]
25	856.2				ļ	. [1	7
26	855.2		j	- 1		1	į	
27	854.2			I	l	I		7
28	853.2			ı	l			1
29	852.2		Ī	I	1	- 1		1
30	851.2			1	l	.		1
31	850.2			1	1			
32	849.2		ļ	1	- 1			ᅦ
33	848.2			l	1	- 1	1	1
34	847.2			<u> </u>		. [1	1
35	846.2		I	l	1	: [1	1
	845.2		1	j	l	1	1	\dashv
36	7		l		l		j	-
37	844.2					- 1	1	4
38-	843.2		- 1	l	I		l	-
"³9∃	842.2	I		1	. 1	- 1		4
40—	841.2	1	1		·	Į		-
41-]	840.2	1		j	l	- 1		4
42 T	839.2 T LEVEL OBSE	DVATIONS:	ADDITIONA	COMMEN	ITS:			
		RVATIONS: None Observed		No groundw		intered wh	ile drilling	or
		None Observed		pon comple				
	epth/Delay:	NA I						
	Caved at:	7± feet (EL 874.2±)						

GENERAL NOTES

SAMPLE IDENTIFICATION

Visual soil classifications are made in general accordance with the Unified Soil Classification System on the basis of textural and particle size categorization, and various soil behavior characteristics. Visual classifications should be substantiated by appropriate laboratory testing when a more exact soil identification is required to satisfy specific project applications criteria.

PAF	<u> TI</u>	CLE	SIZE±	
	_	_		

Boulders:	8 inches	Coarse Sand:		Silt:	0.005 to 0.074 mm
Cobbles:	3 to 8 inches	Medium Sand:		Clay:	-0.005 mm
Gravel:	5 mm to 3 inches	Fine Sand:	0.074 to 0.42 mm		

DRILLING & SAMPLING SYMBOLS

SS: Split-spoon, 2" O.D. b	٧	1	3/8	' I.D.
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ST:	Shelby Tube, 2" O.D. or 3" O.D., as noted in text	RB:	Roller Bit
AU:	Auger Sample	WS:	Wash Sample
DB:	Diamond Bit	BS:	Bag Sample
CB:	Carbide Bit	HA:	Hand Auger

SOIL PROPERTY SYMBOLS

N: Standard penetration count, indicating number of blows of a 140 lb. hammer with a 30 inch drop, required to advance a split-spoon sampler one foot.

Qu: Unconfined compressive strength, tons per square foot (tsf)

Qp: Calibrated hand penetrometer resistance, tsf

MC: Moisture content, %

LL: Liquid Limit

PL: Plastic Limit

PI: Plasticity Index

Dd: Dry Density, pounds per cubic foot (pcf)

PID: Photoionization Detector (Hnu meter) volatile vapor level, ppm

SOIL RELATIVE DENSITY AND CONSISTENCY CLASSIFICATION

NON-COF	HESIVE SOILS		COHESIVE SOIL	.S
Classifier	N-Value Range	Classifier	Qu Range (tsf)	N-Value Range
very loose	0-3	very soft	0-0.25	0-2
loose	3-7	soft	0.25-0.5	2-5
medium dense	7-15	medium stiff	0.5-1.0	5-10
dense	15-38	stiff	1.0-2.0	10-14
very dense	38+	very stiff	2.0-4.0	14-32
,		hard	4.0+	32+

GROUNDWATER



Approximate Groundwater level at time noted on soil boring log, measured in open borehole unless otherwise noted. Groundwater levels often vary with time, and are affected by soil permeability characteristics, weather conditions, & lateral drainage conditions.